

## Hydrodynamische Größen- und Dichtefraktionierung von Mikropartikeln im Serpentina Kanal

### Hydrodynamic size and density fractionation of microparticles in a serpentine channel

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Multi-Dimensional Particle Fractionation, APTV,  $\mu$ PIV, Serpentine Channel Flow

#### Abstract

In the present study, we investigate the size and density fractionation of microparticles in a sharp corner serpentine channel for different bulk Reynolds numbers. To study the 3D dynamics of the particle motion and the flow, Astigmatism Particle Tracking Velocimetry (APTV) and micro Particle Image Velocimetry ( $\mu$ PIV) measurements are combined. Measurement results are compared to numerical results gained by a Lattice Boltzmann Method (LBM).

Results reveal the existence of four spatially separated particle equilibrium trajectories that merge into two particle equilibrium trajectories beyond a critical bulk Reynolds number. Furthermore, we discover spatially separated equilibrium trajectories for Polystyrene (PS) particles of different diameters, as well as for particles of identical diameter but different relative density (Polystyrene and Melamine). The present study provides a proof of principle for multi-dimensional fractionation of bidisperse microparticle systems in a sharp corner serpentine channel.

#### Introduction

The availability of microparticles with well-defined, monodisperse properties is important for several industrial branches, such as metallurgy, food industry or chemical industry. Current developments aim to utilize microfluidic devices to fractionate particles with nominal diameters in the order of  $O(D_p) \approx 10 \mu\text{m}$  [Zhang et al., 2015, Fan et al., 2014, Dincau et al., 2018]. This is because microfluidic devices show an increased selectivity for these particle sizes compared to conventional fractionation methods.

In-plane separation of microparticles of different sizes is observed in serpentine channels by means of time and depth integrated fluorescence imaging. The spatial separation of different particles and their focus on equilibrium trajectories is supposed to develop due to a combination of secondary Dean vortex flow, particle centrifugal forces and inertial migration of particles [Di Carlo, 2009]. An in-plane particle migration towards different equilibrium trajectories is observed for different particle sizes and densities depending on the bulk Reynolds number.

In the present study, we determine the spatial orientation of particle equilibrium trajectories and the corresponding velocity fields by means of  $\mu$ PIV and APTV [Cierpka et al., 2010]. Measured flow fields are furthermore compared to LBM simulations.

In the course of this paper, we show for the first time that a multidimensional fractionation of microparticles with different size and density may be realised in a sharp corner serpentine microchannel.

## Experimental Set-up and Measurement Procedure

Measurements are performed with an EPI-fluorescence microscope (Nikon Eclipse LV100) with an objective lens of  $M_{\text{obj}} = 20$  magnification (20X Nikon CFI60 TU Plan Epi ELWD). The utilized combination of imaging optics results in a total magnification of  $M = 14$ . For particle illumination, a double-pulsed, dual-cavity Nd:YAG laser (Litron Nano S 65-15 PIV) is coupled into the microscope. Particle images are recorded with a CCD double-frame camera (LaVision Imager pro SX) controlled by the LaVision software DaVis 8.4. Astigmatism effects of particle images are generated by inserting a cylindrical lens with a focal length of  $f = 200$  mm in front of the CCD camera.

All measurements are performed downstream in the 24<sup>th</sup> loop of a sharp corner serpentine channel of  $h = 50$   $\mu\text{m}$  height and  $w = 200$   $\mu\text{m}$  width. Different bulk Reynolds numbers  $Re = \frac{u_{\text{max}} \cdot D_h}{\nu}$  are generated with a volume flow controlled syringe pump (HLL LA-800).

Commercial particles (microParticles GmbH) whose properties are listed in Table 1, are used.

**Table 1:** Particle properties.

Diameter $D_P$ [ $\mu\text{m}$ ]	$3.55 \pm 0.07$	$9.89 \pm 0.10$	$9.84 \pm 0.26$
Density $\rho_P$ [ $\text{gcm}^{-3}$ ]	1.05	1.05	1.51
Material	Polystyrene (PS)	Polystyrene (PS)	Melamine (MF)

The flow field is characterised by means of  $\mu$ PIV at different bulk Reynolds numbers. For this, PS tracers with a nominal diameter of  $D_P = 1.19 \pm 0.03$   $\mu\text{m}$  are used. In combination with the imaging optics in use, this results in a depth of correlation of  $z_{\text{corr}} = 15$   $\mu\text{m}$  [Olsen and Adrian, 2000]. In every measurement set, 300 images are recorded at 26 planes equidistantly located over the channel height with a distance of  $\Delta z = 2$   $\mu\text{m}$  in between. Before cross-correlation, all images are pre-processed. A subtract time filter over all images of one recording set is used to reduce background noise, e.g. of particles sticking to the ground. To reduce salt-and-pepper noise, a sliding average filter with Gaussian weighting function of 3 pixels filter length is applied. Afterwards, the ensemble averaged cross-correlations are performed with decreasing interrogation window sizes of  $96 \times 96$  pixels and  $48 \times 48$  pixels with 50% overlap.

To determine the bulk Reynolds number regime, at which differently sized particles undergo a transition from two to one visible equilibrium trajectory, fluorescence images are recorded. For this, particle signals are recorded over 1000 double-frame images and the corresponding particle positions are detected.

The three-dimensional reconstruction of particle positions is performed using an APTV approach. Here, 500 images are recorded at three measurement planes, which have a distance of  $\Delta z = 15$   $\mu\text{m}$  from each other. The measurement depth is found to be always larger than the channel height. APTV recordings are evaluated using a self-written MATLAB code.

## LBM

Micro-PIV measurements are prone to systematic errors, due to a finite correlation depth that covers approximately 30% of the channel height in the present study. Therefore, experimen-

tally derived velocity fields are compared against simulation results, which are gained by utilizing a Lattice Boltzmann Method (LBM). LBM stands out through its simplicity in implementation and its great scalability for parallel processing [Aidun and Clausen, 2010].

It is based on so called density distribution functions  $f$ , which are associated to the grid nodes  $\mathbf{r}$  and the discrete velocities  $e_i$ . Each simulation step is divided into a propagation step, where all the distribution functions are propagated according to their respective velocities and a collision step, where all the distribution functions arriving at one node collide:

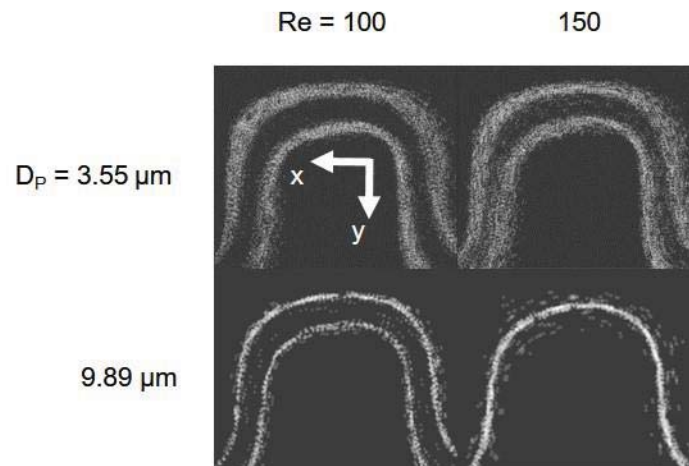
$$|f(\mathbf{r} + \mathbf{e}_i \Delta t, t + \Delta t)\rangle = |f(\mathbf{r}, t)\rangle - \Omega(|f(\mathbf{r}, t)\rangle - |f^{eq}(\mathbf{r}, t)\rangle) + |F\rangle \quad (1)$$

Here  $\Omega$  describes the so called collision operator and  $F$  an optionally applied volume force. There are different approaches to implement the collision operator. We use the Multiple Relaxation Time model on a D3Q19 (three dimensions, nineteen velocities) grid as described in [d'Humieres et al., 2002]. To realize the no slip boundary conditions, we use quadratically interpolated bounce back methods as described in [Bouzidi et al., 2001].

In the present study, all numerical results are performed using periodic boundary conditions in x-direction and a spatial resolution of  $2 \mu\text{m}/\text{node}$ .

## Results and Discussion

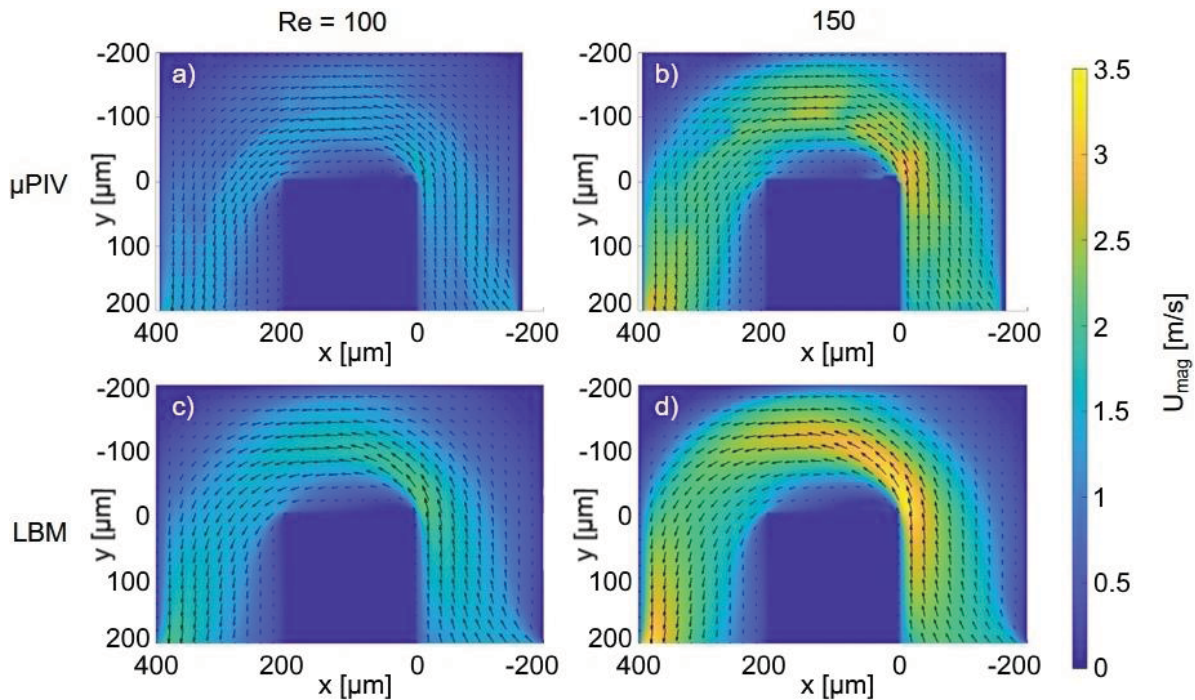
In a first step, the Reynolds number region, at which a transition from two to one visible particle equilibrium trajectory takes place, is identified. This region shifts to higher Reynolds numbers with decreasing particle diameter. Figure 1 shows time integrated particle trajectories of particles with diameters  $D_P = 3.55 \mu\text{m}$  and  $D_P = 9.89 \mu\text{m}$  at bulk Reynolds numbers of  $\text{Re} = 100$  and  $\text{Re} = 150$ . Please note, the overall flow direction takes place in positive x-direction. Here, a transition of particle equilibrium trajectories can be observed for particles of  $D_P = 9.89 \mu\text{m}$ .



**Figure 1:** Particle trajectories for particle fractions with  $D_P = 3.55 \mu\text{m}$  and  $D_P = 9.89 \mu\text{m}$  diameter at bulk Reynolds numbers of  $\text{Re} = 100$  and  $\text{Re} = 150$ .

For a bulk Reynolds number of  $\text{Re} \geq 150$ , spatially separated particle equilibrium trajectories can be observed for  $3.55 \mu\text{m}$  and  $9.89 \mu\text{m}$  particles. Therefore, these two particle groups may be successfully fractionated, if a suitable separation of the fluid streams, containing one of both particle groups, is realized downstream the serpentine channel. This will be discussed in more detail later in this section.

To gain a better insight into the dynamics of particle trajectories, the underlying flow field is characterized. For this,  $\mu\text{PIV}$  measurements are performed and compared to velocity fields resulting from LBM simulations. Figure 2 a) and b) show measured flow fields taken at half the channel height for  $\text{Re} = 100$  and  $\text{Re} = 150$ . These are compared to the simulated velocity fields in Figure 2 c) and d) at the same channel position and bulk Reynolds numbers.



**Figure 2:** Measured (top row) and simulated (bottom row) velocity fields at bulk Reynolds numbers of  $Re = 100$  (left column) and  $Re = 150$  (right column). In the experimental results of a) and b) only every third and in the numeric results of c) and d) only every tenth vector result over the channel width and height is plotted.

The same characteristic features of the experimentally and numerically obtained flow fields are revealed from these exemplary results. Thus, a sharp rise in velocities can be observed at the leading edge of the inner serpentine wall with rising bulk Reynolds number. We assume that this region plays a key role for the migration dynamics of particles, as acceleration, particle centrifugal forces and shear gradient forces on particles are expected to dominate here. Downstream of the edge, a separation region can be observed. It may be noted, that no particle accumulation was observed in this region.

However, to determine relative motions between fluid and particles, the full 3D flow field and particle trajectories need to be determined. A further comparison of the experimental and numerical results shows, that fluid velocities are underestimated in the experiment. This is assumed to result from a relatively large depth of correlation of  $z_{corr} = 15 \mu\text{m}$  present in the  $\mu\text{PIV}$  measurements, spanning about 30% of the channel height. To overcome this, the usage of an APTV approach seems to be feasible.

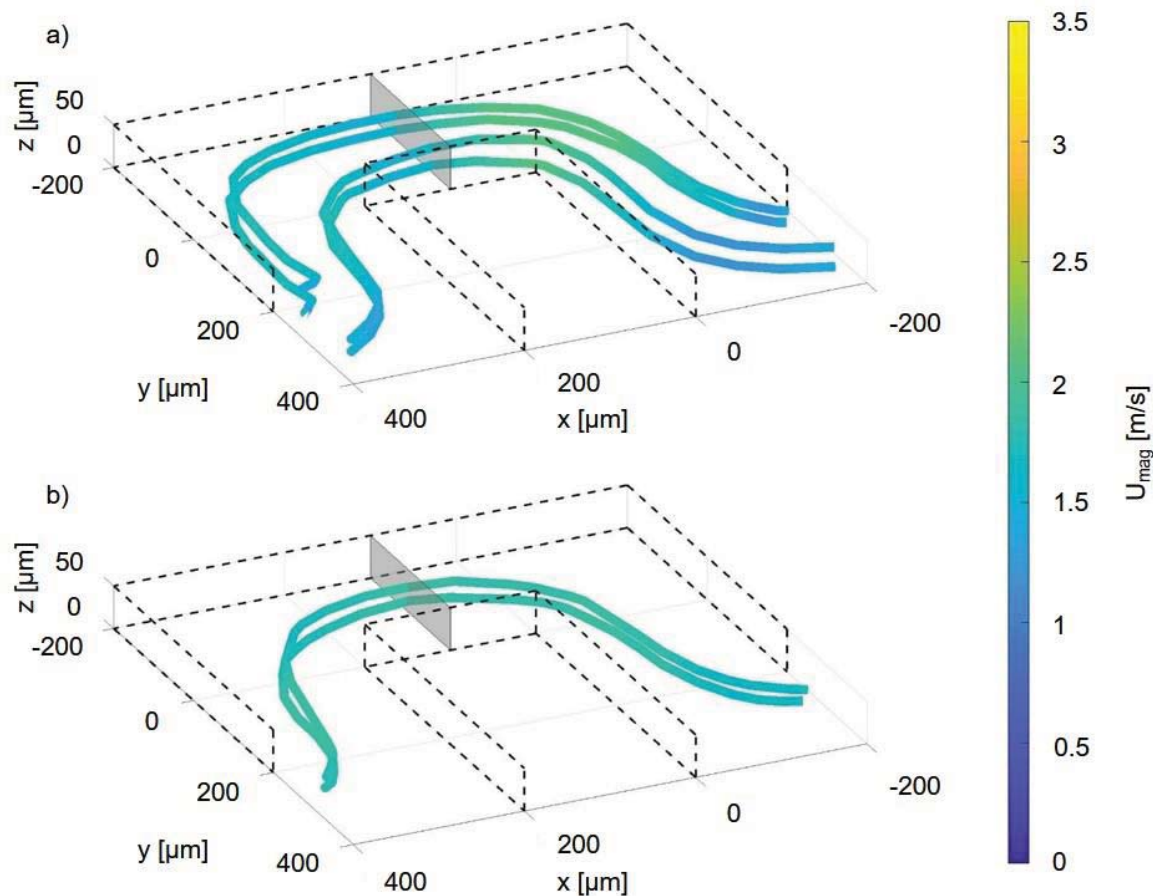
### Size fractionation

In the present study we utilize APTV to reconstruct three-dimensional positions of particle groups from two-dimensional recordings. A parameter study was performed to determine the bulk Reynolds number regime at which the best size fractionation results for PS particles with nominal diameters of  $D_P = 3.55 \mu\text{m}$  and  $D_P = 9.89 \mu\text{m}$  can be expected. For the bulk Reynolds numbers investigated in the present study, best size fractionation results could be achieved at  $Re = 140$ . Corresponding 3D particle trajectories gained from APTV results are shown in Figure 3 a) for  $D_P = 3.55 \mu\text{m}$  and b) for  $D_P = 9.89 \mu\text{m}$ . It is evident, that small particles of  $D_P = 3.55 \mu\text{m}$  diameter undergo significant velocity changes of up to 1 m/s while being transported over half a serpentine loop.

In contrast to this, particles of  $D_P = 9.89 \mu\text{m}$  nominal diameter move with a relatively constant velocity through the serpentine channel, exhibiting only moderate velocity fluctuations in the order of 0.3 m/s. Furthermore, the smaller particle fraction undergoes stronger oscillations over



the channel height while moving through the serpentine channel. A detailed study on fluid forces acting on both particle groups while moving along their equilibrium trajectories is currently in progress.

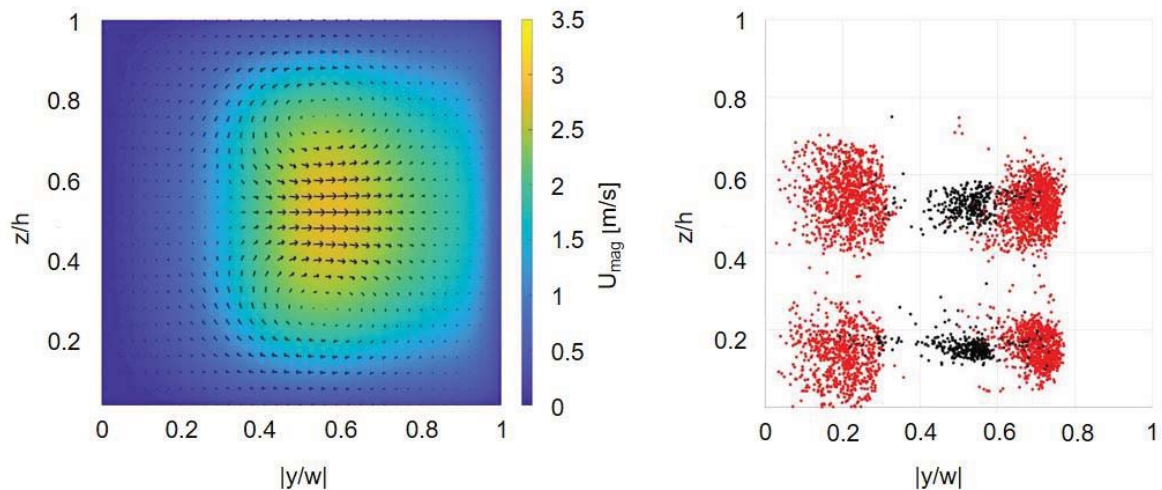


**Figure 3:** APTV results, showing particle centre line trajectories and velocity magnitudes  $U_{mag}$ , at a bulk Reynolds number of  $Re = 140$  of PS particles with nominal diameters of a)  $D_P = 3.55 \mu\text{m}$  and b)  $D_P = 9.89 \mu\text{m}$ .

Figure 4 a) shows the secondary flow motion at  $Re = 140$  derived from simulations in a cross-section that is labelled in grey in Figure 3 a) and b). In y-direction, only every third vector result is shown. Please note, that due to normalisation and for better visualisation, the axis aspect ratios are unified compared to the real channel dimensions.

Figure 4 a) shows the presence of Dean vortices. Their strength maximizes behind the leading edge ( $x=y=0$ ) due to a strong acceleration of the flow that is fostered during the switching of the rotation direction of the secondary flow.

The corresponding particle distributions derived from APTV measurements are indicated in Figure 4 b). Here, particles over a volume depth of  $dx = 200 \mu\text{m}$  are superimposed. Figure 4 b) reveals that four equilibrium positions of particles emerge in the flow. While a spatial separation of particles along the y-direction is known from literature [Zhang et al., 2015], we show here that a clear separation also occurs over the channel height. However, the distribution of different particle groups appears to be axis symmetric with respect to  $z/h = 0.35$ . Therefore, particle fractionation seems feasible only through splitting fluid streams at certain y-positions, for example  $|y/w| = 0.4$  and  $|y/w| = 0.6$  as larger particles (black dots in Figure 4 b) are found near the channel centre between  $0.4 \leq |y/w| \leq 0.6$ , while smaller particles (red dots in Figure 4 b) accumulate between  $0.1 \leq |y/w| \leq 0.2$  and  $0.6 \leq |y/w| \leq 0.8$ .



**Figure 4:** a) Simulated total velocity magnitude and secondary flow normalised with the maximum lateral velocity across the serpentine channel at  $Re = 140$ ; b) Spatial distribution of Polystyrene particles with  $D_p = 3.55 \mu\text{m}$  (red) and  $D_p = 9.89 \mu\text{m}$  (black) diameter at  $Re = 140$ .

The occurrence of particle equilibrium positions can be also observed in a straight, laminar square duct flow for a bulk Reynolds number of  $Re = 144$  and a channel height to particle radius ratio  $h/a = 9$  [Kazerooni et al., 2017]. Depending on the bulk Reynolds number four or eight particle equilibrium positions may occur in a straight channel flow at the wall bisectors or the channel corners.

Therefore, it is assumed that Dean vortices restrict the number of particle equilibrium positions to four positions. However, further studies are required to better understand how finite particle size effects, referred to as inertial migration effects, and particle centrifugal forces interact to induce different particle equilibrium positions as observed in Figure 4 b).

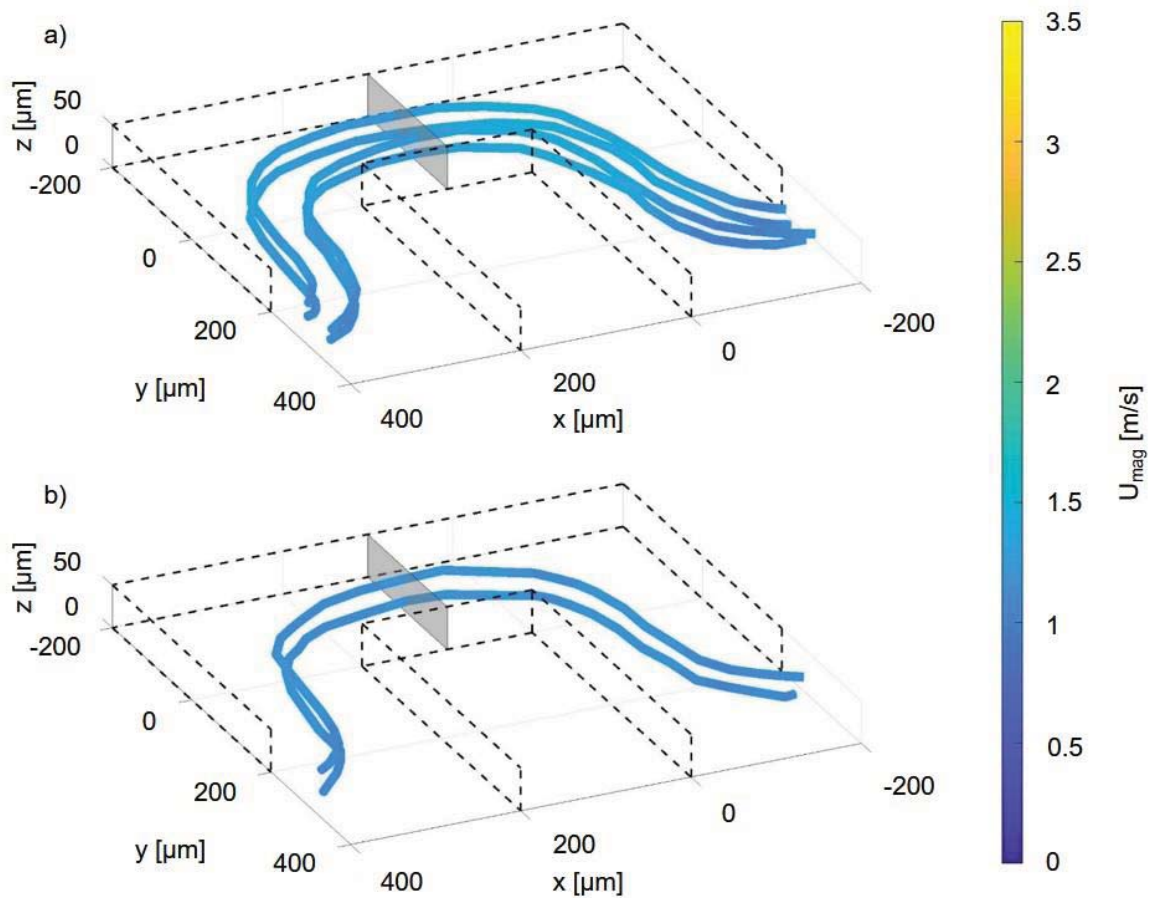
### Density fractionation

While it is known from literature that particles of different sizes may be spatially separated in a sharp corner serpentine channel, we try here for the first time to realize a spatial separation of particles of different densities. Figure 5 a) and b) show sample particle equilibrium trajectories at  $Re = 110$  of PS particles with a nominal diameter of  $D_p = 9.89 \mu\text{m}$  and MF particles with a nominal diameter of  $D_p = 9.84 \mu\text{m}$ . Please note, that only the centre line trajectories are shown in Figure 5 a). For the actual particle spread over the channel width, refer to Figure 6 b).

Figure 5 a) and b) show, that both particle fractions move with a relatively constant velocity of  $1.3 \pm 0.2 \text{ m/s}$  (PS) and  $1.2 \pm 0.1 \text{ m/s}$  (MF), respectively, through the serpentine channel. This is assumed to be a result from increased inertia of relatively large (Figure 5 a) and additionally relatively dense (Figure 5 b) particle fractions.

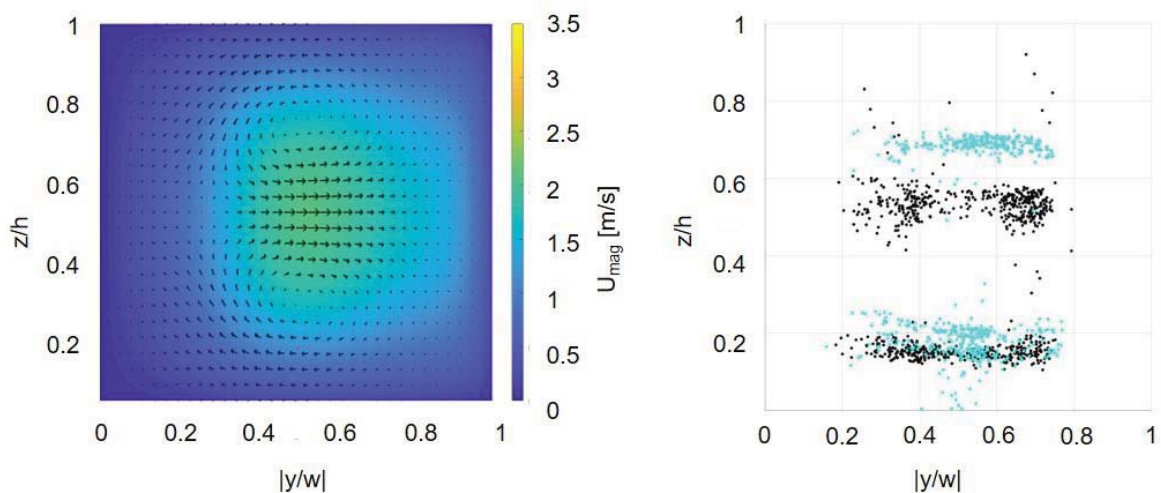
Figure 5 a) and b) show that PS particles merge towards four equilibrium trajectories while heavier MF particles assume two equilibrium trajectories. To investigate options of density fractionation, the exact 3D distribution of particles and the underlying flow field must be known. Figure 6 a) shows simulated velocity results at  $Re = 110$  in a cross-sectional plane (as indicated in grey in Figure 5 a) and b). Even though secondary flow motion is also visible here, Dean vortex strength is decreased by about 42%, compared to the case of  $Re = 140$  (see also Figure 4 a).

In Figure 6 b) the distribution of lighter PS particles (black) and denser MF particles (cyan) at  $Re = 110$  is plotted for a flow volume between  $0 \mu\text{m} \leq x \leq 200 \mu\text{m}$ . As can be noticed, despite the spatial separation of particle centreline trajectories, displayed in Figure 5 a) and b), both PS and MF trajectories are spread in  $y$ -direction.



**Figure 5:** APTV results, showing particle centre line trajectories and velocity magnitudes  $U_{\text{mag}}$ , at a bulk Reynolds number of  $Re = 110$  of a) Polystyrene (PS) particles of  $D_P = 9.89 \mu\text{m}$  diameter and b) Melamine resin (MF) particles of  $D_P = 9.84 \mu\text{m}$  diameter.

That is, because PS particles seem to have just started with the transition process from four to two equilibrium trajectories, while MF particles are more advanced in this transition process. A fractionation by splitting fluid streams in  $y$ -direction seems possible, when separating particles near the channel centre between  $0.4 \leq |y/w| \leq 0.6$  from particles in the outer channel



**Figure 6:** a) Simulated total velocity magnitude and secondary flow normalised with the maximum lateral velocity across the serpentine channel at  $Re = 110$ ; b) Spatial distribution of polystyrene particles with  $D_P = 9.89 \mu\text{m}$  (black) and melamine resin particles with  $D_P = 9.84 \mu\text{m}$  (cyan) diameter at  $Re = 110$ .

regions. However, a separation of fluid streams over the channel height seems to be suitable in future designs, even though more complex to realize technically.

## Conclusion

In the present study, we investigate the capability of a sharp corner serpentine channel to fractionate particles of different sizes and densities for defined particle combinations at different bulk Reynolds numbers. To characterise the flow field, we first performed  $\mu$ PIV measurements and compared the results to LBM simulations. Afterwards, individual particle trajectories were identified by means of APTV.

Up to date, depth-integrated measurements show the existence of one or two particle equilibrium trajectories in lateral channel direction. Here, it is shown for the first time, that spatially separated equilibrium trajectories also evolve over the channel height, leading to a switching between two and four particle equilibrium trajectories.

Particles of different sizes ( $3.55\ \mu\text{m}$  and  $9.89\ \mu\text{m}$ ) could be successfully separated, reaching the best fractionation result at a bulk Reynolds number of  $Re = 140$ . In the case of density fractionation, a separation of PS and MF particles could be observed at a bulk Reynolds number of  $Re = 110$ , although purities of the individual fractions are supposed to be less than in the case of size fractionation. Overall, measurements of 3D particle distributions turn out to be essential for the design of future fractionation devices, as especially for particles with different densities a fractionation over the height might be advantageous.

## Acknowledgement

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